CIVIL ENGINEERING-CE



GATE / PSUs

STUDY MATERIAL STRENGTH OF MATERIALS





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STUDY MATERIAL

STRENGTH OF MATERIALS

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SIMPLE STRESSES AND STRAINS

STRESS (σ):

It is the internal resistance offered by a body against the deformation numerically, it is given as force per unit area.

Stress on elementary area ΔA ,

i.e.
$$\sigma = \lim_{\Delta A \to \Theta} \frac{\Delta F}{\Delta A} = \frac{dF}{dA} (N / m^2)$$
This unit is called

Pa(Pascal)

In case of normal stress dF always \perp (perpendicular) to

area dA.

Pascal is a small unit in practice. These units are generally used

 $1 kPa = 10^{3} Pa = 10^{3} N/m^{2}$ $1 MPa = 10^{6} Pa = 10^{6} N/m^{2}$ $1 GPa = 10^{9} Pa = 10^{9} N/m^{2}$



1. Normal Stress: It may be tensile or compressive depending upon the force acting on the material.

Tensile and compressive stresses are called direct stresses.

When, $\sigma > 0$, Tensile

When, $\sigma < 0$, Compressive

> The other types of normal stress is bending normal stress.



Bending stress are linearly distributed from zero at neutral axis to maximum at surface.

In bending, the cross-sectional area rotates about transverse axis and the axis about which the cross-sectional area rotates is called neutral axis hence in bending, neutral axis is always transverse axis.

2. Shear Stress (τ): It is the intensity of shear resistance along a surface (Let X-X).

$$\tau = \frac{Shear \ force}{Shear \ Area} \left| (N/m^2) \right|$$

In case of shear stress force always parallel to the sheared area *i.e.* P is parallel to sheared area in figure.



3. Conventional or Engineering Stress (σ_0): It is defined as the ratio of load (P) to the original area of crosssection (A₀):

$$\therefore \qquad \sigma_0 = \frac{P}{A_0}$$

4. True Stress (σ): It is defined as the ratio of load (P) to the instantaneous area of cross-section (A):

$$\therefore \qquad \sigma = \frac{P}{A} \text{ or, } \overline{\sigma = \sigma_0(1 + \varepsilon)} \text{ Where } \varepsilon = \text{strain } \begin{bmatrix} Al = A_0 l_0 \\ l = l_0(1 + \varepsilon) \end{bmatrix} \text{ Initial volume = Final volume}$$

STRAINS (ε):

•

It is defined as the change in length per unit length. It is a dimensionless quantity.



1. Conventional or Engineering strain: It is defined as the change in length per unit original length.

$$\varepsilon = \frac{l - l_0}{l_0}$$

Where,

l = Deformed length

 l_0 = Original length

e.g. from above figure.

$$\varepsilon = \frac{l+dl-l}{l} \qquad \varepsilon = \frac{dl}{l}$$

2. Natural Strain: It is defined as the change in length per unit instantaneous length.

$$\overline{\varepsilon} = \int_{l_0}^{l} \frac{dl}{l} = n \frac{l}{l_0} \quad l \neq (1 \quad \mathfrak{F} + \ln\left(\frac{A_0}{\overline{A}}\right) - 2\ln\left(\frac{d_0}{\overline{d}}\right)$$
Also, $\because \quad \overline{\varepsilon} = \ln(1+\varepsilon)$

Also, $\because \quad \varepsilon = \ln (1 + \varepsilon)$ $\Rightarrow \quad 1 + \varepsilon = e^{\overline{\varepsilon}}$ $\Rightarrow \quad \varepsilon = e^{\overline{\varepsilon}} - 1$

Volume of the specimen is a assumed to be constant during plastic deformation \therefore $A_0L_0 = AL$ -Valid till neck formation.

3. Shear Strain (ϕ): It is the strain produced under the action of shear stresses.



Shear Strain = $tan \phi$

For small strain, $\tan \phi \approx \phi$

From figure, $\triangle ACC'$ or $\triangle BDD'$

$$\tan\phi = \frac{dl}{l} = \frac{CC'}{l}$$

dl	Transverse displacement
$\left \begin{array}{c} \psi - \overline{l} \\ l \end{array} \right $	Distance from lower face

> Shear strain cause deformation in shape but volume remains same.

4. Superficial strain (ε_s): It is defined as the change in area of cross section per unit original area.

$$\varepsilon_s = \frac{A - A_0}{A_0}$$

SOM

- $A_0 = \text{Original area}$
- 5. Volumetric Strain (ε_v) : It is defined as the change in volume per unit original volume.

$$\varepsilon_V = \frac{V - V_0}{V_0}$$

Where, V = Final volume V_0 = Original volume

Stress and strain are tensor (neither vector nor scalar) of 2nd order. \succ

Volumetric strain $\varepsilon_{V} = \varepsilon_{x} + \varepsilon_{y} + \varepsilon_{z}$

Volumetric strain for various shapes:



(*i*) Rectangular body:

V = lbh on partial differentiation

$$\delta V = \delta l(b.h) + \delta b(l.h) + \delta h(b.l)$$
$$\varepsilon_{V} = \frac{\delta V}{V} = \frac{\delta l}{l} + \frac{\delta b}{b} + \frac{\delta h}{h}$$
$$\varepsilon_{V} = \varepsilon_{x} + \varepsilon_{y} + \varepsilon_{z}$$

Note: $\varepsilon_x, \varepsilon_y, \varepsilon_z$ are the strain corresponding to the stresses $\sigma_x, \sigma_y, \sigma_z$ in x-direction, y-direction, z-direction

respectively

$$\varepsilon_{\rm v} = \frac{\sigma_x + \sigma_y + \sigma_z}{\rm E} (1 - 2\upsilon) \qquad \qquad \mu \quad -\text{Poisson Ratio}$$

 $\mu = 0.5$ For rubber

(ii) For cylindrical body:

$$\mathbf{V} = \frac{\pi}{4}d^2l$$

$$\delta V = 2 \, dl \cdot \delta d \cdot \frac{\pi}{4} + \frac{\pi}{4} d^2 \delta l$$
$$\varepsilon_{\rm V} = \frac{\delta V}{V} = 2 \frac{\delta d}{d} + \frac{\delta l}{l}$$
$$\varepsilon_{\rm V} = 2\varepsilon_d + \varepsilon_l$$

(iii) For spherical body

Gauge Length: It is that portion of the test specimen over which extension or deformation is measured. i.e. this length is used in calculating strain value.

Poisson's ratio $\left(\mu \text{ or } \frac{1}{m}\right)$: Value of μ varies between (-1 to 0.5)

The ratio of the lateral strain to longitudinal strain is called the Poisson's ratio.



- > For a given material, the value of ' μ ' is constant throughout the linearly elastic range.
- For most of the metals the value of ' μ ' lie between 0.25 0.42
- \succ ' μ ' varies from (-1 to 0.5)

Note: ' μ ' for ductile material is greater than ' μ ' for brittle metals.

Table

Material	Value of 'µ'	Remarks
Cork	0	: Used in bottle to withstand pressure
Foam	-1	
Rubber	0.5	
Concrete	0.1 - 0.2	
C.I.	0.23 - 0.27	

For cork	μ	Ð	
For rubber	μ	₽ .5	
For concrete	и	₽ .1	0-2

Isotropic Material: These materials have same elastic properties in all directions.

No. of independent elastic constants = 2, *i.e.* if any of 2 elastic constants is known then other can be derived.

Orthotropic Material: The number of independent elastic constants is 9.

Anisotropic materials: These materials don't have same elastic properties in all directions.

Elastic modulii will vary with additional stresses appearing. ... There is a coupling between shear stress and normal stress for an isotropic material.

The number of independent elastic constants is 21.

Hooke's Law: It states that when a material is loaded such that the intensity of stress is within a certain limit, the ratio of the intensity of stress to the corresponding strain is a constant which is characteristics of that material.

Note: The certain limit is called proportionality limit but for most practical purposes, proportionality limit equals elastic limit.

i.e. $\frac{\text{Stress}}{\text{Strain}} = \text{Constant} = E$ *i.e.*, $\sigma = E \varepsilon$

Where, E = Young's Modulus (N/m²)

Or

Modulus of Elasticity

- For steel, value of E = 210 GPa (1 GPa = 10^3 N/m²)
- ➤ For aluminum, value of E = 73 GPa $E_{AI} \simeq \frac{1}{3}$ rd E_{steel}
- \blacktriangleright For Plastic, value of E = 1 GPa 14 GPa

Note : As flexibility increases, value of young's modulus decreases.

It is resistance to elastic strain.

Shear Modulus of Elasticity OR Modulus of Rigidity (G or C): It is defined as the ratio of shearing stress to shearing strain.

$$G \text{ or } C = \frac{Shear \text{ stress}}{Shear \text{ strain}} \text{ i.e. } \tau = G \varphi$$

Bulk Modulus (K):

It is defined as the ratio of uniform stress intensity to volumetric strain within the elastic limits.

$$K = \frac{\text{Normal Stress}}{\text{Volumetric Strain}}$$

Note: Elastic constant relationship

(i) E = 2C(1 + u), where, v = Poisson's ratio.

(ii)
$$E = 3K(1 - 2\mu)$$

(iii)
$$\mu = \frac{3K - 2C}{6K + 2C}$$

(iv)
$$E = \frac{9KC}{3K+C}$$

STRESS-STRAIN DIAGRAM:

I. Ductile material (Mild Steel):



Figure: Typical stress-strain diagram for a ductile material

> Point 'a' \rightarrow Limit of proportionality: Up to this point 'a', Hooke's law is obeyed; 'oa' is a straight line.

Stress corresponding to this point is called 'proportional limit stress, σ_p '

Comparison of Engineering and true stress strain curve:

- The true stress-strain curve is also known as **flow curve**.
- True stress-strain curve gives a true indication of deformation characteristics because it is **based on the**

instantaneous dimension of specimen.

- In engineering stress-strain curve, the stress drops down after necking since it is based on the original area.
- In true stress strain curve, the stress however increases after necking since the cross section area of the specimen **decreases rapidly after necking.**

• The flow curve of many metals in the region of uniform plastic deformation can be expressed by **simple power law**.

$$\sigma_{\mathrm{T}} = \mathrm{K}(\in_{\mathrm{T}})^n$$

where, K is the strength co-efficient, σ_{T} is time stress.

n is the strain hardening coefficient.

n = 0 for perfectly plastic solid

n = 1 In elastic solid

For most metals 0.1 < n < 0.5

 $\sigma_{\text{True}} > \sigma_{\text{Nominal}} \rightarrow \text{ if force is tensile, since area decreases.}$

 $\sigma_{True} > \sigma_{Nominal} \rightarrow$ if force is compressive, since area increase.



> Relation between ultimate tensile strength and true stress at maximum load.

Ultimate tensile strength $\sigma_u = \frac{P_{max}}{A_o}$

True stress at maximum load = $(\sigma_u)_T = \frac{P_{max}}{A}$



True strain at max load
$$(\varepsilon_{T}) = \ln \frac{A_{o}}{A}$$
 or $\frac{A_{o}}{A} = e^{\varepsilon_{T}}$
Eliminating P_{max} we get

 $(\sigma_u)_{\mathrm{T}} = \frac{\mathrm{P}_{\mathrm{max}}}{\mathrm{A}} \times \frac{\mathrm{A}_o}{\mathrm{A}_o}$ $= \frac{\mathrm{P}_{\mathrm{max}}}{\mathrm{A}_o} \times e^{\varepsilon_{\mathrm{T}}}$ $\implies (\sigma_u)_{\mathrm{T}} = \sigma_u e^{\varepsilon_{\mathrm{T}}}$

Here, P_{max} is the max force.

 A_{a} = original cross section area

- A = instantaneous cross section area
- Based on the above theory two examples has been provided.

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